Quantum computers can execute certain algorithms exponentially faster than their classical counterparts, such as Shor’s factoring algorithm.1–3 This is achieved by creating exponentially faster than their classical counterparts, such as Shor’s factoring algorithm.1–3 This is achieved by creating superconducting approaches to quantum computing hold great promise, due to the relatively good performance displayed by superconducting qubits, combined with the ease with which complex superconducting integrated circuits can be fabricated. This is witnessed by a number of recent publications describing beautiful multi-qubit experiments implemented in superconducting architectures.4–8

Scaling up to larger numbers of qubits is however a significant challenge, in part because each qubit must be separately controlled and measured. Any simplification or reduction in the resources needed to implement control or measurement would provide an important advantage. In this Letter, we describe a multiplexed qubit readout scheme for the superconducting phase qubit that promises highly efficient scaling, a scheme that is also applicable to other qubit systems.

A phase qubit’s quantum state is measured by the process illustrated in Fig. 1(a). A current pulse is applied to the qubit, lowering the barrier between the metastable computational energy well (marked L for left well) and the minimum energy well (marked R for right well). The qubit excited state |e⟩ selectively tunnels from the left into the right well, where its energy relaxes, while the ground state |g⟩ stays in the left well. Following this projective measurement, the outcome is determined by reading out in which well the qubit resides. The readout is typically done using a superconducting quantum interference device (SQUID), which can distinguish between the values of magnetic flux that correspond to the left and right wells, and can thus identify whether the qubit was projected onto the |g⟩ or the |e⟩ state.

This readout scheme has high single-shot fidelity (typically better than 90%), and protects the qubit from dissipative effects associated with some other readout schemes.9 However, there are some deleterious effects, including the generation of excess quasiparticles from switching to the voltage state of the SQUID,10 and the need for more complex fabrication, as the readout circuits involve fabricating three SQUID Josephson junctions for each qubit. To overcome some of these problems, dispersive microwave readout schemes have been developed for the phase qubit,11,12 in which either the qubit itself or an adjacent SQUID modulates the scattering parameters of a nearby microwave transmission line. These techniques eliminate the generation of quasiparticles, but limit the qubit performance by adding
decoherence from the direct connection to the transmission line, or still require SQUID co-fabrication, respectively.

Here, we replace the readout SQUID with a lumped-element readout resonator that is weakly coupled to the qubit and to a nearby readout transmission line, as shown in Fig. 1(b). This significantly simplifies fabrication, eliminates quasiparticles and other heating effects, and maintains good qubit coherence. The projective measurement is the same as that of the SQUID readout, but the result is read out by measuring the effective inductance of the qubit Josephson junction. Each qubit is coupled to its readout resonator through a mutual inductance $M$, such that it presents an effective parallel inductance $\Delta L$ to the resonator, given by

$$\Delta L = \frac{-M^2}{L + zL_J}, \quad (1)$$

where $L$ is the qubit loop inductance, $L_J$ is the effective Josephson inductance, and $z = 1 - f^2/f_0^2 \approx 0.8$ is a detuning factor that depends on the microwave probe frequency $f$. For the device here, $f \approx 4$ GHz and $f_0 = 1/2\pi\sqrt{L/C} \approx 6.5$ GHz, determined by the qubit parallel inductance $L$ and capacitance $C$. The effective Josephson inductance $L_J$ has a different value when the qubit is in the left or in the right well. The readout resonator frequency is $\tilde{f} = 1/2\pi\sqrt{C_R(L_R + \Delta L)}$, where $C_R$ and $L_R$ are the resonator capacitance and inductance, respectively. Thus, the readout resonator frequency depends on the qubit state through $L_J$, so the phase of a probe signal reflected off the resonator will also depend on whether the qubit is in the left or right well.

We demonstrated the multiplexed readout using a quantum circuit comprising four phase qubits and five integrated resonators, shown in Fig. 1(c). The design of this chip is similar to that used for a recent implementation of Shor’s algorithm,5 but here the qubits were read out off a single line using microwave reflectometry, replacing the SQUID readout used in Ref. 8. This dramatically simplifies the chip design and significantly reduces the footprint of the quantum circuit. We designed the readout resonators so that they resonated at frequencies of 3-4 GHz (far de-tuned from the qubit $|g\rangle \leftrightarrow |e\rangle$ transition frequency of 6-7 GHz), with loaded resonance linewidths of a few hundred kilohertz. This allows us to use frequency multiplexing, which has been used in the readout of microwave kinetic inductance detectors13,14 as well as other types of qubits.15,16 Combined with custom GHz-frequency signal generation and acquisition boards, this approach provides a compact and efficient readout scheme that should be applicable to systems with 10-100 qubits using a single readout line, with sufficient measurement bandwidth for microsecond-scale readout times.

As the readout was performed by measuring the reflection off a single transmission line, some care was taken in the microwave design in order to avoid standing waves from reflections. This included designing the coupling capacitor values and adjusting the lengths of the readout lines between successive resonators; for example, the readout line has an extra bend between qubits $Q_2$ and $Q_3$.

We used a standard heterodyne detection method to measure the reflected signal from each readout resonator, as shown in Fig. 2. Key components include two customized field-programmable gate array (FPGA) boards, one connected to two 14-bit digital-to-analog converters (DACs) for generating arbitrary probe waveforms, with a 1 GS/s digitizing rate (GS/s: gigasample per second), and the other connected to two 8-bit analog-to-digital converters (ADCs) for data acquisition and processing, also with a 1 GS/s digitizing rate. Probe waveforms were generated by preparing multitone signals in both $I_p$ and $Q_p$ (cosine and sine) probe quadratures for mixer up-conversion, each tone chosen so that after frequency up-conversion in an IQ mixer, it matched the resonance frequency $f_n$ ($n = 1-4$ corresponding to the readout resonator for qubits 1–4) of the readout resonators. The reflected signals were amplified and down-converted with a second IQ mixer; the reflected $I_n(t)$ and $Q_n(t)$ signals comprised the same signal tones as the probe waveform, but with an additional phase shift that encodes the measurement signal, i.e., the phase $\phi_n$ of the reflected tone at frequency $\tilde{f}_n$ encodes the state of the qubit $n$. The phases $\phi_n$, $n = 1-4$, were then evaluated using the digital demodulation channel on the data acquisition FPGA board. This was performed by digital mixing and integrating of the digitized $I_n(t)$ and $Q_n(t)$ signals at the resonator frequency $\tilde{f}_n$, each with a separate demodulation channel.

The optimization of the readout process was done in two steps. We first optimized the microwave probe frequency to maximize the signal difference between the left and right well states. This was performed by measuring the reflected phase $\phi$ as a function of the probe frequency, with the qubit prepared first in the left and then in the right well. In Fig. 3(a), we show the result with the qubit flux bias set to 0.15 $\Phi_0$, where the difference in $L_J$ in two well states was relatively large. The probe frequency that maximized the signal difference was typically mid-way between the loaded resonator frequencies for the qubit in the left and right wells, marked by the dashed line in Fig. 3(a). We typically obtained resonator frequency shifts as large as $\sim$150 kHz for the qubit between the two wells, as shown in Fig. 3(a), significantly larger than the resonator linewidth.

With the probe frequency set in the first step, the flux bias was then set to optimize the readout. As illustrated in

![Fig. 2. Setup for frequency-multiplexed readout. Multiplexed readout signals $I_p$ and $Q_p$ from top FPGA-DAC board are up-converted by mixing with a fixed microwave tone, then pass through the circulator into the qubit chip. Reflected signals pass back through the circulator, through the two amplifiers $G1$ and $G2$, and are down-converted into $I_r$ and $Q_r$ using the same microwave tone, and are then processed by the bottom FPGA-ADC board. Data in the shadowed region are the down-converted $I_r$ and $Q_r$ spectra output from the FPGA-ADC board; probe signals from the FPGA-DAC board have the same frequency spectrum. D.C. indicates the digital demodulation channels, each processed independently and sent to a computer.](image323x632 to 553x755)
Using the optimal probe frequency and flux bias, this readout scheme can distinguish between $|g\rangle$ and $|e\rangle$ with a measurement fidelity of about 90%, somewhat less than we typically achieve with a SQUID readout. The qubit energy decay time was measured to be $T_1 \approx 600$ ns and the dephasing time $T_\phi \approx 150$ ns, for all the qubits. These are typical values for our phase qubits, indicating that replacing the readout SQUID with a resonator did not introduce any significant additional decoherence.

With the readout process optimized for each qubit, we demonstrated the frequency-multiplexed readout by performing a multi-qubit experiment. To minimize crosstalk, we removed the coupling capacitors between qubits used in Ref. 8. In this experiment, we drove Rabi oscillations on each qubit’s $|g\rangle \rightarrow |e\rangle$ transition and read out the qubit states simultaneously. We first calibrated the pulse amplitude needed for each qubit to perform a $|g\rangle \rightarrow |e\rangle$ Rabi transition in 10 ns. The drive amplitude was then set to 1, 2/3, 1/2, and 2/5 the calibrated Rabi transition amplitude for qubits Q1 to Q4, respectively, so that the Rabi period was 20 ns, 30 ns, 40 ns, and 50 ns for qubits Q1 to Q4. We then drove each qubit separately using an on-resonance Rabi drive for a duration $\tau$, followed immediately by a projective measurement and qubit state readout. This experiment yielded the measurements shown in Figs. 4(a)–4(d) for qubits Q1–Q4.

With each qubit individually characterized, we then excited and measured all four qubits simultaneously, as shown in Fig. 4(e). There is no measurable difference between the individually measured Rabi oscillations in panels (a)-(d) compared to the multiplexed readout in panel (e).

In summary, we have demonstrated a frequency-multiplexed qubit readout scheme for superconducting phase qubits. Using a single excitation and readout line, with a single amplifier chain, we can measure four qubits simultaneously, without sacrificing measurement bandwidth or qubit coherence. This technology can be scaled up to readout simultaneously tens to hundreds of qubits, greatly aiding the scaling-up of quantum circuits to larger numbers of qubits.
This work was supported by IARPA under ARO Award No. W911NF-08-01-0336 and under ARO Award No. W911NF-09-1-0375. M.M. acknowledges support from an Elings Postdoctoral Fellowship. R.B. acknowledges support from the Rubicon program of the Netherlands Organisation for Scientific Research. Devices were made at the UC Santa Barbara Nanofabrication Facility, a part of the NSF funded National Nanotechnology Infrastructure Network.